

	1
	3
	ز-'
	4.
	C
Walter ACEST	
view or many a Commence of the	
A. C. Nine, Ceptain, USN Tourney Ministry Company Officer	•,
	-
	D
도 사용하는 경우의 1842년 등 교육이 되었다. 그런 이 기를 수 있는 것이 되었다. 	
- The Hard (2) (1) (1) (1) (1) (1) (1) (1) (1) (1) (1	C
	<b>-</b> ,
	,
	ر
	<b>.</b> 3
	ing F
;	

# **Executive Summary**

Water depths in the near-shore zone of western Isla de Vieques are calculated using Landsat 4 Thematic Mapper imagery and two different algorithms. The first is a new algorithm that does not require a sea-bottom-type clustering; the second is the dual-band-ratio algorithm. TM bands one and two (0.45–0.52  $\mu m$  and 0.52–0.60  $\mu m$ , respectively) are water penetrating and provide capability for calculating water depths to about 20 m in clear water. A comparison of results of remotely sensed bathymetry using  $\partial \Omega$  two different models is made.

# Acknowledgments

This work was performed by the Naval Ocean Research and Development Activity and sponsored by the Office of Naval Technology, program element 62435N, Oceanographic Support Block RM035G85, under the direction of Dr. H. C. Eppert.

### **Contents**

Introduction	1
Background	1
Procedure	2
Results and Analysis	2
Applications	3
References	3



Arices	o For	
titio	ou loca	<b>3</b> 000
By Distric	otion)	
μ	vallations	Circles
U'st	Avar in d Specia	-
A-/		į

### A Comparison of Models for Remotely Sensed Bathymetry

#### Introduction

Remotely sensed bathymetry from multispectral imagery has been studied for several years. Three models have been devised to enable calculation of water depth, the so-called single-band algorithm, the two-band ratio method, and the multiband method. The first two models have the disadvantage of requiring a bottom-type clustering to minimize the bottom reflectance variation. The third model requires many (>2) water-penetrating bands, because present sensors are predominantly optimized for land remote sensing and do not have sufficient water-penetrating bands to satisfy this model.

The single-band algorithm and the dual-band ratio method have been tested with good results. <sup>7,9</sup> However, a new algorithm we call the linear multiband method has recently been introduced <sup>10</sup> that does not require a bottom-type clustering. This new algorithm holds the promise of yielding absolute bathymetry in cases where the number of different bottom types is equal to or less than the number of water-penetrating bands in the imagery.

We recently tested the linear multiband method using bands one and two of Landsat Thematic Mapper imagery in the vicinity of Isla de Vieques. The results are compared to bathymetric measurements made using the dual-band ratio method. The calibration data used in both methods were taken from a 1:25000 combat chart of the region. With the linear multiband algorithm we achieved improved results without performing the time-consuming process of bottom-type clustering and classification required by the dual-band ratio model.

### **Background**

Remotely sensed bathymetry from multispectral imagery generally is based upon a simple reflectance model; the radiance in wavelength band i at water depth z is given by

$$L_i = L_{i\infty} + c_i R_{ai} \exp(-2k_i Z),$$

where  $L_i$  is the radiance value in band i,  $L_{i\infty}$  is the average signal over deep water,  $c_i$  is a constant that is a function of several optical parameters,  $R_{ai}$  is the bottom reflectance in band i over bottom type a, and  $k_i$  is the diffuse attenuation coefficient.

Solving for z, one obtains the formula

$$Z = LN (c_i R_{ai}) / 2k_i - X_i / 2k_i$$

where we have adopted the convention that  $X_i = LN(L_i - L_{\infty})$ .

This single-band reflectance model assumes that the bottom reflectance is constant over the bottom type, that the atmosphere and the sea state are uniform, and that other background optical effects are either uniform or constant throughout the image.

To reduce errors due to the variation of the bottom reflectances, a two-band ratio method (or dual-band method) was devised.<sup>5</sup> In this algorithm, the depth is given by

$$Z = (1/2 (k_1 - k_2)) (LN (c_1 R_{a1} c_2 R_{a2}) + X_1 - X_2)$$

where the subscripts I and 2 indicate different bands. In this method, we assume that changes in the bottom reflectances occur in such a way that the ratio  $c_1R_{al}/c_2R_{al}$  remains constant.

Another method, which we call the linear multiband method, gives the depth by

$$Z = \sum \omega_i (1/2k_i) (LN(c_i R_{ai}) - X_i)$$

where the sum is taken over several bands and the weights  $\omega_i$  satisfy the constraint that  $\Sigma \omega_i = I$ . Paredes and Spero, generalizing the assumption that the ratio  $c_1R_{al}/c_2R_{a2}$  remains constant, assume there are constants  $s_i$  and  $\alpha$  independent of bottom type such that

$$(c_1R_{a1})^{\zeta_1}(c_2R_{a2})^{\zeta_2}(c_3R_{a3})^{\zeta_3} \dots =$$

$$(c_1R_{h_1})^{\zeta_1}(c_2R_{h_2})^{\zeta_2}(c_3R_{h_3})^{\zeta_3} \dots =$$

With this assumption, they show that certain weights,  $\omega_i$  can be found such that, when used in the above multiband linear depth equation, produce an equation for Z independent of the bottom reflectance and depend only upon the values  $S_i$ :

$$Z = (1/2\sum_{\varsigma_i}k_i)(1-\varsigma_1X_1-\varsigma_2X_2\cdots).$$

Alternatively, this equation may be written

$$Z = A_0 + A_1 X_1 + A_2 X_2 + \dots + A_n X_n$$

where the coefficients  $A_0$ ,  $A_1$ , ...,  $A_n$  are constants independent of the bottom type at which the depth is being calculated. (See ref. 7 for more details.)

It has been shown that the assumption underlying the two-band ratio method is not satisfied by Landsat TM data<sup>7</sup> and it has been suggested<sup>7</sup> that the linear multiband algorithm, with the generalized ratio assumption, may be more accurate given more bands than bottom classes, as the coefficients in the algorithm do not depend on the bottom reflectance. In this paper we use the linear multiband algorithm on two channels of a Landsat 4 TM scene and demonstrate its improved performance over the two-band ratio method.

#### **Procedure**

The Landsat scene used in this study (scene number 5032614162, taken January 21, 1985) contains Isla de Vieques, an island off the southeast coast of Puerto Rico in the Carribean Sca. The water clarity in this area is extremely good, and bottom reflectances in the blue and green channels (TM bands one and two) are detectable for depths up to 25 m. Bottom reflectances in the red channel (TM band three) are detectable for depths up to about 6 m; sensor noise (striping) over the water renders this band useless at greater depths.

The general procedure for this comparison of the three methods was first to convert a National Aeronautics and Space Administration/Goddard Space Flight Center computer compatible tapes to an image data file and to georeference this data file against a Defense Mapping Agency 1:25000 combat chart. See reference 8 for details on the georeferencing procedure. This combat chart contains not only bathymetric soundings, but also land feature identifications that aid in the georeferencing process. A set of approximately 600 calibration points was then selected by recording depths from the chart; about 300 of the points were used in our regression fit and the remaining 300 were used as a test set to check the calculated depth against the actual depth.

The average deep-water signal for each waterpenetrating band (in this case channels 1 and 2, roughly corresponding to the blue-green and green portions of the visible spectrum, respectively) was calculated to obtain the  $L_{im}$  values.

Polygons were drawn on the image to outline the deep water (no visible ocean bottom) region in each band. The average intensity of the pixels contained in the polygon was used as the  $L_{i\infty}$  values. These values are subtracted from the corresponding  $L_i$  value to adjust the signal values for atmospheric scattering, etc.

A linear regression of the model equation against the (appropriate) calibration points is run, which produces coefficients and, hence, equations for the depth Z at any pixel. The test set of calibration points is used to test the fit of this regression. These equations are then used to produce a bathymetric image that can be processed further (smoothed, contoured, pseudocolored, etc.) depending upon the desired application.

#### **Results and Analysis**

The linear regression was run on the equation

$$Z = A_0 + A_1 X_1 + A_2 X_2$$

corresponding to a two-channel multiband linear model. For this image we determined  $L_{i\infty}=68$  and  $L_{2\infty}=17$ . The regression yielded the following values for the constants:  $A_0=11.2, A_1=3.14, A_2=-6.76$  The multiple correlation coefficient was 0.86.

Scatter plots indicated an apparent correlation of error with depth, so we plotted the test residuals of measured depth versus calibration depth for three different depth ranges, 0-5 m, 5-10 m, and 10-16 m. Residual means and RMS values are given in Table 1. It was seen that we consistently underestimated the depth in the shallower water and overestimated the depth in the deeper water.

Using the test set of calibration point data, the model yielded an overall residual mean less than  $0.2\,\text{m}$  and an overall RMS less than  $1.9\,\text{m}$ . Performing the regression in the depth range of  $0-5\,\text{m}$ , the RMS error was  $0.88\,\text{m}$ ; in the range  $5-10\,\text{m}$ , the RMS error was  $1.25\,\text{m}$ ; and in the range  $10-16\,\text{m}$ , the RMS error was  $1.00\,\text{m}$ .

For comparison purposes, the dual-band ratio method was applied as well. To minimize error, the image was clustered to locate areas of similar bottom reflectance using a supervised statistical clustering routine and the maximum likelihood classifier. The algorithm was then regressed against calibration points in each cluster separately. An overall residual mean of 0.093 m and an RMS error of 2.66 m was obtained (Table 2). In the depth range of 0-5 m, the RMS error was 0.94 m; in the range 5-10 m, the RMS error was 1.56 m; and in the range 10-15 m, the RMS error was 1.86 m.

Table 1. Errors in depth calculation from linear multiband model.

Residual Mean	RMS
0.002 m	0.88 m
- 0.39 m	1.25 m
- 0.21 m	1.00 m
0.20 m	1.86 m
	- 0.39 m - 0.21 m

Table 2. Errors in depth calculation from dual-band ratio model.

Depth Range	Residual Mean	RMS
0 – 5 m	0.12 m	0.94 m
5 – 10 m	- 0.15 m	1.56 m
10 –15 m	- 0.25 m	1.86 m
0 – 15 m	0.10 m	2.66 m

In comparing the two methods, both algorithms underestimated the depth in shallow water and overestimated it in deeper water. This tendency produces a larger overall error than is obtained when considering the indicated depth ranges. It can be seen that the linear multiband method yields somewhat improved results, even when only two bands are available. Moreover, this method does not require the clustering and classification routines to discern areas of similar bottom reflectance, and a considerable savings in CPU processing time (one to several hours on a VAX 11/780 per 512 X 512 pixel image) is realized.

#### **Applications**

A major advantage of calculating water depths from remotely sensed data is the reduction in preparation time and in the cost of producing bathymetric charts. Moreover, the digital nature of the product lends itself to easy and rapid editing and updating.

The extrapolation of calculated bathymetric coefficients from one portion of a scene to another portion is easily accomplished due to the digital nature of the data. The authors intend to study the validity of such extrapolations in future work as this has the potential of being a major mapping, charting, and geodesy application.

#### References

- 1. Polcyn, F. C., D. R. Lyzenga, F. J. Tanis. *Demonstration of Satellite Bathymetric Mapping*, Environmental Research Institute of Michigan, Report #122200-1-F, Ann Arbor, Michigan, January 1977
- 2. Hammack, J., Landsat Goes to Sea, *Photogrammetric Engineering and Remote Sensing*, vol. 43, p. 683, 1977.
  3. Polcyn, F. C., and R. Lyzenga, Remote Bathymetry of the Shallow Seas by Satellite, presented at the *Symposium on Measurement*, *Mapping*, and *Management in the Coastal Zone*, May 21–22, 1979.
- 4. Jerlov, N. G., Optical Oceanography, Elsevier, New York, 1976.
- 5. Polcyn, F. C., W. L. Brown, and I. J. Sattinger, *The Measurement of Water Depth by Remote Sensing Techniques*, Report 8973-26-F, Willow Run Laboratories, The University of Michigan, Ann Arbor, 1970.
- 6. Lyzenga, D. R., Passive Remote Sensing Techniques for Mapping Water Depth and Bottom Features, *Applied Optics*, vol. 17, p. 379, 1978.
- 7. Paredes, J. M. and R. E. Spero, Water Depth Mapping from Passive Remote Sensing Data Under a Generalized Ratio Assumption, *Applied Optics*, vol. 22, p. 1134, 1983
- 8. Clark, R. K., T. H. Fay, C. L. Walker, Bathymetry Measurements from Landsat Imagery in the Vicinity of Isla de Vieques, Naval Ocean Research and Development Activity, Report 202, NSTL, Mississippi, 1988.
- 9. Clark, R. K., T. H. Fay, and G. E. Terrie, Coastline Extraction and Beach Width Definition, Naval Ocean Research and Development Activity, Report 149, NSTL, Mississippi, 1986.
- 10. Clark, R. K., T. H. Fay, and R. T. Joy, Bathymetry from Multispectral Digital Data, Proceedings of the Second Annual Symposium of the Gulf Coast Chapter of the National Hydrographic Society, NSTL, Mississippi, September 1986, in press.
- 11. Clark, R. K., T. H. Fay, C. L. Walker, Applications of Multispectral Imagery to the Production of MC&G Products, Proceedings of the Annual Defense Mapping Agency Conference on Mapping, Charting, and Geodesy, Washington, D.C., October 1986.
- 12. Clark, R. K., T. H. Fay, C. L. Walker, Bathymetry Calculations from Landsat TM Imagery Under a Generalized Ratio Assumption, accepted for publication in *Applied Optics*, vol. 26, p. 4036, 1987.

#### DISTRIBUTION LIST

002 A1 FCTS ASN(RE&S) Department of the Navy Asst Secretary of the Navy (Research Engineering & System) Washington DC 20350-1000

004 A3 FCTS CNO Department of the Navy Chief of Naval Operations Attn: OP-951 Washington DC 20350-2000

Director
National Oceanic Data Center
WSC1 Room 103
6001 Executive Blvd
Attn: G. W. Withee
Rockville MD 20852

004 A3 FCTS CNO Department of the Navy Chief of Naval Operations Attn: OP-987 Washington DC 20350-2000

005 A3 FCTS CNO Oceanographer of the Navy Chief of Naval Operations Attn: OP-096 U.S. Naval Observatory 34th & Mass Ave., NW Washington DC 20390-1800

006 1303 500 E3D2 FCTS NAVAIRDEVCEN Commander Navai Air Development Center Warminister PA 18974-5000

007 1461 900 FKA1A FCTS COMNAVAIRSYSCOM Commander Naval Air Systems Command Headquarters Washington DC 20361-0001

009 2130 600 E3D3 FCTS NAVCOASTSYSCEN Commanding Officer Naval Coastal Systems Center Panama City Ft. 32407-5000

023 2925 905 FKA1B FCTS COMSPANAVWARSYSCOM Commanding Officer Space & Naval Warfare Sys Com Washington DC 20363-5100

030 2980 500 E3D11 FCS NAVENVPRESRSCHFAC Commanding Officer Naval Environmental Prediction Research Facility Monterey CA 93943-5006

031 3075 910 FKA1C FCTS COMNAVFACENGCOM Commander Naval Facilities Eng Command Headquarters 200 Stovall St. Alexandria VA 22332-2300

045 4488 200 E3C FCTS NORDA Commanding Officer Naval Ocean R&D Activity Attn: Code 100 NSTL MS 39529-5004 045 4488 200 E3C FCTS NORDA Commanding Officer Naval Ocean R&D Activity Attn: Code 1251 (13) NSTL MS 39529-5004

045 4488 200 E3C FCTS NORDA Commanding Officer Naval Ocean R&D Activity Atm: Code 125P (1) NSTL MS 39529-5004

045 4488 200 E3C FCTS NORDA Commanding Officer Naval Ocean R&D Activity Attn: Code 105 NSTL MS 39529-5004

045 4488 200 E3C FCTS NORDA Commanding Officer Naval Ocean R&D Activity Attn: Code 211 NSTL MS 39529-5004

045 4488 200 E3C FCTS NORDA Commanding Officer Naval Ocean R&D Activity Attn: Code 200 NSTI MS 39529-5004

045 4488 200 E3C FCTS NORDA Commanding Officer Naval Ocean R&D Activity Attn: Code 300 NSTL MS 39529-5004

047-3860-930-E3A-FCS-NRI Commanding Officer Naval Research Laboratory Washington DC 20375

053 4480 100 FD1 FCS MCAFA/OCEANAV Commander Naval Oceanography Command NSTL MS 39529-5000

059 4483 270 FD3 FCTS FLENUMOCEANEN Commanding Officer Fleet Numerical Ocean Center Monterey CA 93943-5065

062 4485 365 LD2 FCTS MCAFA 'NAVOCEANO Commanding Officer Naval Oceanographic Office NSTL MS 39522-5001

065 4489 800 E3D4 FCTS NAVOCEANSYSCOM Commander Naval Ocean Systems Center San Diego CA 92152-5000

068 5580 350 E3B FCS ONRBRO Commanding Officer ONR Branch Office Box 39 FPO New York 09510-0700

i

071 5856 900 E3D6 FCTS DTNSRDC Commander DWTaylor Naval Research Center Bethesda MD 20084-5000

074 6214 950 E3D7 FCTS NAVSWC Commander Naval Surface Warfare Center Dahlgren VA 22448-5000

076 6541 500 FCTS E3D9 NUSC Commanding Officer Naval Underwater Systems Center Newport RI 02841-5047

085 7685 435 FT73 FCTS NAVPGSCOL Superintendent Naval Postgraduate School Monterey CA 93943

098 5520 750 C4L FCS ONL Director of Naval Laboratories Space and Naval Warfare Sys Com Washington DC 20363-1451

131 C20J FCTS NUSCDET Officer in Charge Naval Underwater Sys Cen Det New London CT 06320

136 B2A FCS DTIC Defense Technical Info Cen Attn: DTIC-DDAC (12) Cameron Station Alexandria VA 22314

298 A2A FCTS ONR Director Office of Naval Research 800 N. Quincy St. Code 10 Arlington VA 22217-5000

800 WHOI FCS CONT Director Woods Hole Oceanographic Inst P. O. Box 32 Woods Hole MA 02543

304 SCRIPPS FCS CONT Director University of California Scripps Institute of Oceanography PO Box 6049 San Diego CA 92106

376 C201 FCTS NAVSURWPNCEN Officer in Charge White Oak Laboratory Naval Surface Warfare Center Det 10901 New Hampshire Ave Attn: Library Silver Spring MD 20903-5000

034 3135 550 FT46 FCTS Commanding Officer Fleet Anti-Sub Warfare Training Center Atlantic Naval Station Norfolk VA 23511-6495 Brooke Farquhar NORDA Liaision Office Room 802 Crystal Plaza #5 2211 Jeff Davis Hwy Arlington VA 22202-5000

Hudson Institute Center for Naval Analyses P. O. Box 16268 Alexandria VA 22302

Commander Naval Space Command Dahlgren VA 22448-5170

Director Defense Mapping Agency Washington DC 20305

Defense Mapping Agency Hydrographic/Topographic Center 6500 Brooke Lane Washington DC 20315

Defense Mapping Agency Special Program Office of Explortation & Modernization 8301 Greensboro Drive, Suite 800 McLean VA 22102

University of South Alabama University Station Mobile AL 36688

University of Southern Mississippi Hardy St. Hattiesburg, MS 39401

Director Defense Intelligence Agency Attn: DC-5B (B. Gordon) Washington DCL 20340-0001

Dept of Navy Chief of Naval Operations Attn: OP-943 Washington DC 20350

Commanding Officer Naval Avionics Center 6000 East 21st Street Indianapolis IN 46219-2189

Commandant of the Marine Corps Hdqrs Attn: DIRINT U.S. Marine Corps Washington DC 20380

U.S. Army Engineer and Topographic Lab FT. BELVOIR, VA 22060

Commanding General Marine Corps Development & Education Command Quantico VA 22134

Dep CG
Marine Corps Research &
Development & Acquisition
Attn: C21
Quantico VA 22134

REPORT DOCUM	ENTATION PAGE				
Ta REPORT SECURITY CLASSIFICATION	T 16 RESTRICTIVE MARKINGS				
Unclassified	None				
2a SECURITY CLASSIFICATION AUTHORITY	3 DISTRIBUTION: AVAILABILITY	OF REPORT			
26 DECLASSIFICATION/DOWNGRADING SCHEDULE	Approved for publ unlimited.	ic release; dis	tribution is		
4 PERFORMING ORGANIZATION PUPORT NUMBER(S)	5 MONITORING ORGANIZATION	REPORT NUMBERIS			
NORDA Report 145	NORDA Report 14	<b>4</b> 5			
6 NAME OF PERFORMING ORGANIZATION	74 NAME OF MONITORING ORGANIZATION				
Naval Ocean Research and Development Activity					
6c ADDRESS (City State, and ZIP Code)	76 ADDRESS-City State and	TIP Code:			
Ocean Science Directorate NSTL, Mississippi 39529-5004	Ocean Science Directorate NSTL, Mississippi 39529-5004				
Ba NAME OF FUNDING/SPONSORING ORGANIZATION Bb OFFICE SYMBOL Naval Ocean Research and Development Activity	a PROCHEMENT INSTRUMENT IDENTIFICATION NUMBER				
8c ADDRESS (City State and ZIP Code.	19 SOURCE OF FUNDING NOS				
Ocean Science Directorate NSTL, Mississippi 39529-5004	PROGRAM PROJE ELEMENT NO NO 62435N RM0	NO	NO		
11 TITLE (Include Security Classification)					
A Comparison of Models for Remotely Sensed B	ithymetry				
12 PERSONAL AUTHORIS:  R. Kent Clark*, Temple H. Fay**, Charles L. Wa	ker				
13a TYPE OF REPORT 13b TIME COVERED	14 DATE OF REPORT IT MO	Dav	15 PAGE COUNT		
Final From To	August 1987		6		
** SUPPLEMENTARY NOTATION **University of South Alabama, Mobile, AL and ***University of Southern Mississippi, Hattiesburg, MS					
	rinue on reverse 7 necessary and				
dual-band-ratio	Viegues, Landsat, Thematic Mapper imagery, ind-ratio algorithm, bathymetry, multispectral y, optical bathymetry				
19 ABSTRACT Continue on reverse if impessate and identify by block number		<del>`</del>			
Water depths in the near-shore zone of western Isla de Vieques are calculated using Landsat 4. Thematic Mapper imagery and two different algorithms. The first is a new algorithm that does not require a sea-bottom-type clustering; the second is the dual-band-ratio algorithm. TM bands one and two (0.45–0.52µm and 0.52–0.60 µm, respectively) are water penetrating and provide capability for calculating water depths to about 20 m in clear water. A comparison of results of remotely sensed bathymetry using the two different models is made.					
ZU DISTRIBUTION/AVAILABILITY OF ABSTRACT	21 ABSTRACT SECURITY CLAS	SIFICATION			
UNCLASSIFIED/UNLIMITED CAME AS RPT   DTIC 'USERS	Unclassified				
			22c OFFICE SYMBOL  Code 351		

DD FORM 1473, 83 APR

EDITION OF 1 JAN 73 IS OBSOLETE

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE